

PCT

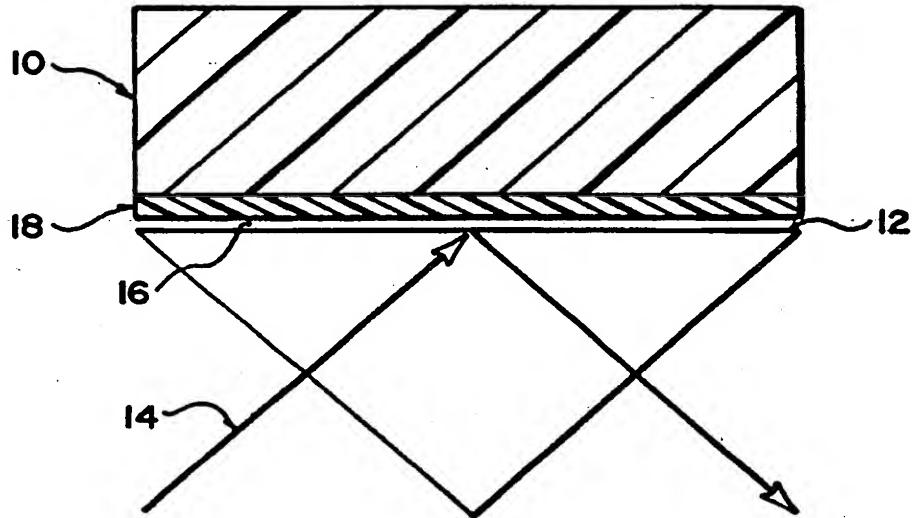
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International Bureau



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(54) Title: METHOD AND APPARATUS FOR CONTROLLABLE FRUSTRATION OF TOTAL INTERNAL REFLECTION



(57) Abstract

A method and apparatus for facilitating controllable switching an interface (12) between a reflective state in which light (14) incident upon the interface undergoes total internal reflection, and a non-reflective state in which total internal reflection is prevented at the interface. The apparatus incorporates a member (10 – preferably an elastomer) which is deformable with respect to the interface. The member's Young's Modulus in portions (18) of the member adjacent the interface is substantially greater (i.e. stiffer) than the member's Young's Modulus in portions of the member away from the interface. The stiffened portion of the member adjacent the interface may be in the form of a microstructure (20). A pair of electrodes (22, 24) coupled to a voltage source can be provided to controllably deform the member into optical contact with the interface, within a continuously variable range of optical contact values, to produce the non-reflective state in selectively varying degrees.

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METHOD AND APPARATUS FOR CONTROLLABLE  
FRUSTRATION OF TOTAL INTERNAL REFLECTION

Technical Field

5        This application pertains to a method and apparatus for frustrating the phenomenon of total internal reflection in a continuously variable, easily controllable manner.

Background

10       It is well known that light travels at different speeds in different materials. The change of speed results in refraction. The relative refractive index between two materials is given by the speed of an incident light ray divided by the speed of the refracted ray. If the relative  
15       refractive index is less than one, then light will be refracted towards the surface, e.g. light emerging from a glass block into air. At a particular angle of incidence "i", the refraction angle "r" becomes  $90^\circ$  as the light runs along the block's surface. The critical angle "i" can be  
20       calculated, as  $\sin i = \text{relative refractive index}$ . If "i" is made even larger, then all of the light is reflected back inside the glass block and none escapes from the block. This is called total internal reflection. Because  
25       refraction only occurs when light changes speed, it is perhaps not surprising that the incident radiation emerges slightly before being totally internally reflected, and hence a slight penetration (roughly one micron) of the interface, called "evanescent wave penetration" occurs. By interfering with (i.e. scattering and/or absorbing) the  
30       evanescent wave one may prevent (i.e. "frustrate") the total internal reflection phenomenon.

      In a number of applications, it is desirable to controllably frustrate the phenomenon of total internal reflection. For example, if total internal reflection is  
35       occurring at an interface "I" as shown in Figure 1A, the degree of reflection can be reduced by placing a dielectric material close to interface I such that dielectric D interacts with the evanescent wave penetrating beyond interface I, as shown in Figures 1B, 1C, and 1D, in which the extent

of frustration of total internal reflection is gradually increased, culminating in complete frustration (Figure 1D).

It is desirable that dielectric D be an elastomeric material. Inevitably, at least some foreign particles "P"

5 (Figure 2A) are trapped between dielectric D and interface I; and/or, the opposing surfaces of dielectric D and interface I have at least some dimensional imperfections "X" (Figure 2B) which prevent attainment of a high degree of surface flatness over substantial opposing areas of both

10 surfaces. Such foreign particles, or such surface imperfections, or both, can prevent attainment of "optical contact" between dielectric D and interface I. Optical contact brings dielectric D substantially closer than one micron to interface I, thereby scattering and/or absorbing

15 the evanescent wave adjacent interface I, thus preventing the capability of interface I to totally internally reflect incident light rays. If dielectric D is formed of an elastomeric material, the aforementioned adverse effects of such foreign particles and/or surface imperfections are

20 localized, thereby substantially eliminating their impact on attainment of the desired optical contact. More particularly, as seen in Figures 2C and 2D, the elastomeric nature of dielectric D allows dielectric D to closely conform itself around foreign particle P and around surface

25 imperfection X, such that optical contact is attained between dielectric D and interface I except at points very close to foreign particle P and around surface imperfection X. Since such points typically comprise only a very small fraction of the opposing surface areas of dielectric D and

30 interface I, sufficiently substantial optical contact is attained to facilitate frustration of total internal reflection as described above.

However, if an elastomeric material makes optical contact with a surface, the elastomeric material tends to stick to that surface and it is difficult to separate the two. This is because elastomeric materials are sufficiently soft that the material can deform into intimate

atomic contact with the atomic scale structure present at any surface; and, because the resultant Van der Waals bonds have sufficient adhesion that it is difficult to remove the material from the surface. These factors make it difficult 5 to use an elastomeric material to frustrate the total internal reflection phenomenon; and, they make it especially difficult to use an elastomeric material to control or vary the degree of total internal reflection. It is desirable to control the degree of frustration of total 10 internal reflection by varying an interfacial pressure applied between dielectric D and interface I; and, in general, it is desirable to achieve such control with the least possible amount of pressure. The aforementioned Van 15 der Waals bonding can require negative pressures of order  $10^4$  Pascals for release, which is desirably reduced. The present invention addresses the foregoing concerns.

#### Summary of Invention

The invention facilitates controllable switching of an 20 interface between a reflective state in which light incident upon the interface undergoes total internal reflection, and a non-reflective state in which total internal reflection is prevented at the interface. This is achieved by providing an apparatus having a member which is 25 deformable with respect to the interface. The member's Young's Modulus in portions of the member adjacent the interface is substantially greater than the member's Young's Modulus in portions of the member away from the interface. More particularly,  $E > a/d$ , where E is the 30 member's Young's Modulus at portions of the member adjacent the interface, a is the bond energy per unit area due to the Van der Waals force between the interface and the member, and d is a dimension characteristic of roughness of the interface. Preferably, the member's Young's Modulus at 35 portions of the member adjacent the interface is greater than about  $10^6$  Pascals.

Advantageously, the member is an elastomer (preferably a silicone elastomer), although it is not essential for the member to be an elastomer; it is sufficient for the bulk dielectric material to be a reasonably flexible substance, 5 such as Teflon™. The portions of the member adjacent the interface may be in the form of a microstructure on a face of the elastomer. Means such as a pair of electrodes coupled to a voltage source can be provided to controllably deform the member into optical contact with the interface, 10 within a continuously variable range of optical contact values, to produce the non-reflective state.

The invention further provides a method of stiffening a selected surface portion of a (typically elastomer) member whereby the member's Young's Modulus in the selected 15 portion is substantially increased with respect to the member's Young's Modulus in portions of the member other than the selected portion, the method comprising irradiating the selected portion with ultraviolet light. Advantageously, the irradiating step is performed in the presence 20 of oxygen.

Another method is to apply a non-adhesive polymer coating having a preselected stiffness to a microstructured film, then apply elastomer to the polymer-coated microstructured film, and then dissolve the film, leaving the 25 stiffened microstructure adherent to the elastomer.

#### Brief Description of Drawings

Figures 1A, 1B, 1C and 1D show various stages in frustration of the total internal reflection phenomenon at 30 interface I as dielectric D is gradually moved toward interface I.

Figures 2A and 2B respectively depict a foreign particle P and a surface imperfection X preventing attainment of optical contact between interface I and dielectric 35 D. Figures 2C and 2D respectively depict attainment of substantial optical contact between interface I and dielec-

tric D notwithstanding foreign particle P or surface imperfection X if dielectric D is an elastomeric material.

Figure 3A depicts a stiff-surfaced elastomeric dielectric positioned adjacent an interface in accordance with 5 one embodiment of the invention. Figure 3B depicts a stiff-surfaced, microstructured elastomeric dielectric positioned adjacent an interface in accordance with a further embodiment of the invention. Figure 3C is similar 10 to Figure 3B and shows a pair of electrodes for controllably deforming the microstructured elastomeric dielectric toward the adjacent interface.

Figure 4 is a graph on which percentage reflectivity is plotted as a function of pressure applied between the elastomeric dielectric and the interface of Figure 3.

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#### Description

Figure 3A depicts an elastomeric dielectric 10 positioned adjacent interface 12. Light rays 14 incident upon interface 12 are totally internally reflected because air 20 gap 16 between the opposing surfaces of dielectric 10 and interface 12 is large enough to prevent optical contact between the opposing surfaces (i.e. gap 16 is substantially greater than one micron). As hereinafter explained, the Young's Modulus  $E$  of dielectric 10 varies as a function of 25 distance from the surface of dielectric 10 adjacent interface 12, such that the portion 18 of dielectric 10 near the surface is substantially stiffer than in the remaining portions of dielectric 10.

The stiffened surface portion 18 of dielectric 10 prevents 30 attainment of the aforementioned Van der Waals bonding between dielectric 10 and interface 12, since such bonding occurs only if dielectric 10 is sufficiently deformable. Roughly speaking, the Young's Modulus of a material (a measure of the material's stiffness) must be 35 less than the Van der Waals bond energy per unit area divided by a characteristic dimension associated with the material's surface roughness, in order for substantial

atomic contact to occur. For surfaces which are sufficiently smooth to exhibit total internal reflection, in which the characteristic dimension of the roughness is substantially less than one micron, sticking will occur if the Young's Modulus is less than about 10<sup>6</sup> Pascals, which is the case for elastomeric materials. Hence, by increasing the Young's Modulus of elastomeric dielectric 10 at the surface of dielectric 10 one may stiffen that surface sufficiently to prevent sticking.

10 The aforementioned surface stiffening should be such that the surface of dielectric 10 can assist in achieving a predictable, reproducible degree of frustration of total internal reflection which varies as function of the pressure applied between dielectric 10 and interface 12.

15 Preferably, under low positive interfacial pressure, there is very little frustration of total internal reflection, and air gap 16 retains a well defined average value of slightly over one micron. This is important, particularly if the interfacial pressure is to be created by electrostatic force, as such narrow air gaps can support large fields due to the "Paschen effect", and these large fields can be produced with fairly low voltages, due to the small gap.

25 One method of creating the desired surface characteristics in elastomeric dielectric 10 is to prepare a uniform, smooth-surfaced elastomeric material, and then treat that material in a manner which stiffens and/or textures a thin surface portion of the material. One acceptable technique is to irradiate the surface of a 30 silicone elastomer with ultraviolet light. Although not wishing to be bound by any theory, the inventors note that such irradiation is typically performed in the presence of oxygen, so it may be that the combination of the ultraviolet light and the resultant ozone are important. The 35 effect may be to increase cross-linking of polymer chains near the treated surface of the elastomer material, in-

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creasing the Young's Modulus in this region. However the precise nature of the effect(s) involved is uncertain.

Another method is to separately apply a thin layer of stiff material to the surface of an elastomeric material. 5 More particularly, a sacrificial microstructured film is coated with a thin non-sticky polymer having a preselected stiffness. One way of making such a coating is to spin cast liquid poly-methyl-methacrylate ("PMMA") which then polymerizes to yield a sub-micron thick coating; while 10 another way is to vacuum deposit parylene on the film. Elastomer is then cast against the PMMA. The sacrificial film is then dissolved by a solvent which does not attack the coating or the elastomer, leaving the microstructured surface adherent to the elastomeric material. Figure 3B 15 depicts such a stiffened microstructured surface 20 bonded to elastomeric dielectric 10.

A further desirable property of the Figure 3B structure is that gradual increase of the pressure will yield gradual frustration of total internal reflection. This is 20 illustrated in Figure 3C, which depicts a first electrode 22 bonded between stiffened microstructured surface 20 and the remaining flexible portion of dielectric 10; and, a second electrode 24 bonded to interface 12. A voltage source "V" is electrically coupled between electrodes 22, 25 24. By suitably varying the voltage applied between electrodes 22, 24 one may deform dielectric 10 and its stiffened microstructured surface 20 toward interface 12 within a continuously variable range of optical contact values, thereby attaining any desired degree of frustration 30 of the capability of interface 12 to totally internally reflect incident light rays. Figure 4 graphically illustrates the resultant range of reflectivity.

As will be apparent to those skilled in the art in the light of the foregoing disclosure, many alterations and 35 modifications are possible in the practice of this invention without departing from the spirit or scope thereof. For example, although dielectric 10 is preferably a sili-

cone elastomer, it need not necessarily be an "elastomer"; it is sufficient for the bulk dielectric material to be a reasonably flexible substance, such as Teflon™. Accordingly, the scope of the invention is to be construed in accordance with the substance defined by the following claims.

## WHAT IS CLAIMED IS:

1. Apparatus for controllably switching an interface (12) between a reflective state in which light (14) incident upon said interface undergoes total internal reflection and a non-reflective state in which said total internal reflection is prevented at said interface, said apparatus characterized by a member (10) deformable with respect to said interface, said member's Young's Modulus in portions (18) of said member adjacent said interface being substantially greater than said member's Young's Modulus in portions of said member away from said interface.  
5
2. Apparatus as defined in claim 1, wherein  $E > a/d$ , where  $E$  is said member's Young's Modulus at portions of said member adjacent said interface,  $a$  is the bond energy per unit area due to the Van der Waals force between said interface and said member, and  $d$  is a dimension characteristic of roughness of said interface.  
10
3. Apparatus as defined in claim 1, wherein said member's Young's Modulus at portions of said member adjacent said interface is greater than about  $10^6$  Pascals.  
15
4. Apparatus as defined in claim 1, wherein said member is an elastomer.  
20
5. Apparatus as defined in claim 1, wherein said member is a silicone elastomer.  
25
6. Apparatus as defined in claim 4, wherein said portions of said member adjacent said interface further comprise a microstructure (20) on a face of said elastomer.  
30
- 35

- 10 -

7. Apparatus as defined in claim 4, further comprising means for deforming said elastomer into optical contact with said interface to produce said non-reflective state.  
5
8. Apparatus as defined in claim 7, wherein said deforming means deforms said elastomer to leave a separation distance between said elastomer and said interface of substantially less than .5 microns and substantially more than  $10^4$  microns.  
10
9. Apparatus as defined in claim 7, further comprising control means (22, 24) for controlling said elastomer deformation within a continuously variable range of optical contact values.  
15
10. A method of stiffening a selected surface portion of a member whereby said member's Young's Modulus in said selected portion is substantially increased with respect to said member's Young's Modulus in portions of said member other than said selected portion, said method characterized by irradiating said selected portion with ultraviolet light.  
20
11. A method as defined in claim 10, further comprising performing said irradiating step in the presence of oxygen at said selected portion.  
25
12. A method as defined in claim 10, wherein said member is an elastomer.  
30
13. Apparatus as defined in claim 10, wherein said member is a silicone elastomer.
14. A method of stiffening a selected surface portion of a member, said method characterized by the steps of:  
35

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- (a) applying a non-adhesive polymer coating having preselected stiffness to a microstructured film;
- (b) applying said member to said polymer-coated film; and,
- 5 (c) dissolving said film, leaving said stiffened microstructure adherent to said member.

15. A method as defined in claim 14, wherein said coating step further comprises spin casting liquid poly methyl methacrylate onto said microstructured film.

10

16. A method as defined in claim 14, wherein said coating step further comprises vacuum depositing parylene onto said microstructured film.

15

17. A method as defined in claim 14, wherein said dissolving step further comprises applying to said member and to said polymer-coated film a solvent which dissolves said film without degrading said member or said micro-structure.

20

18. A method as defined in claim 14, wherein said member is an elastomer.

25

19. Apparatus as defined in claim 14, wherein said member is a silicone elastomer.

**AMENDED CLAIMS**

[received by the International Bureau on 16 February 1999 (16.02.99);  
original claims 1-19 replaced by new claims 1-8  
(3 pages)]

1. Apparatus for controllably switching an interface (12) between a reflective state in which light (14) incident upon said interface undergoes total internal reflection and a non-reflective state in which said total internal reflection is prevented at said interface, said apparatus characterized by a member (10) deformable with respect to said interface, said member's Young's Modulus in portions (18) of said member adjacent said interface being substantially greater than said member's Young's Modulus in portions of said member away from said interface, wherein  $E > a/d$ , where  $E$  is said member's Young's Modulus at portions of said member adjacent said interface,  $a$  is the bond energy per unit area due to the Van der Waals force between said interface and said member, and  $d$  is a dimension characteristic of roughness of said interface.
2. Apparatus for controllably switching an interface (12) between a reflective state in which light (14) incident upon said interface undergoes total internal reflection and a non-reflective state in which said total internal reflection is prevented at said interface, said apparatus characterized by an elastomer member (10) deformable with respect to said interface, said member's Young's Modulus in portions (18) of said member adjacent said interface being substantially greater than said member's Young's Modulus in portions of said member away from said interface, wherein said portions of said member adjacent said interface further comprise a microstructure (20) on a face of said elastomer.

3. Apparatus for controllably switching an interface (12) between a reflective state in which light (14) incident upon said interface undergoes total internal reflection and a non-reflective state in which said total internal reflection is prevented at said interface, 5 said apparatus characterized by an elastomer member (10) deformable with respect to said interface, said member's Young's Modulus in portions (18) of said member adjacent said interface being substantially greater than said member's Young's Modulus in portions of said member away from said interface, further comprising means for deforming said elastomer into optical contact with said interface to produce said non-reflective state, and control means (22, 24) for controlling said elastomer deformation within 10 a continuously variable range of optical contact values.

15 4. A method of making a stiffened microstructure on a selected surface portion of a member, said method characterized by the steps of:

(a) applying a non-adhesive polymer coating having preselected stiffness to a microstructured film;

20 (b) applying said member to said polymer-coated film; and,

(c) dissolving said film, leaving said stiffened microstructure adherent to said member.

25 5. A method as defined in claim 4, wherein said coating step further comprises vacuum depositing parylene onto said microstructured film.

6. A method as defined in claim 4, wherein said dissolving step further comprises applying to said member and to said polymer-coated film a solvent which dissolves said film without degrading said member or said microstructure.

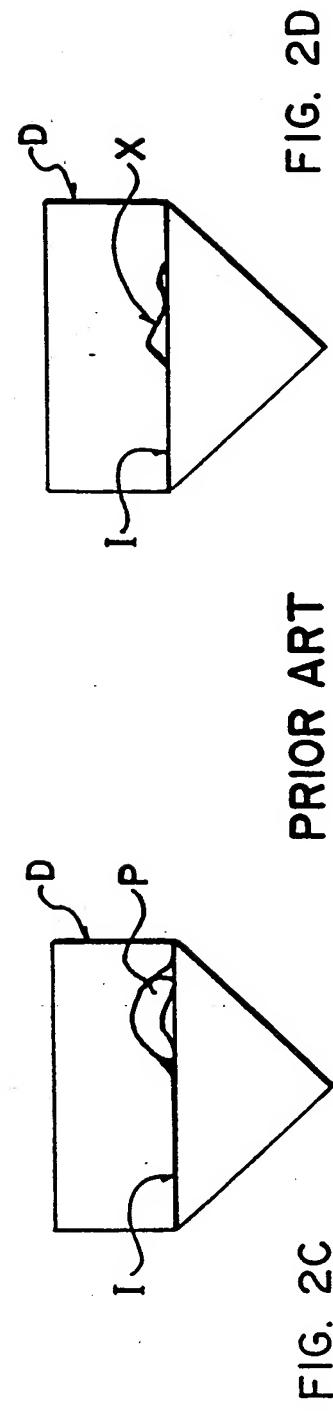
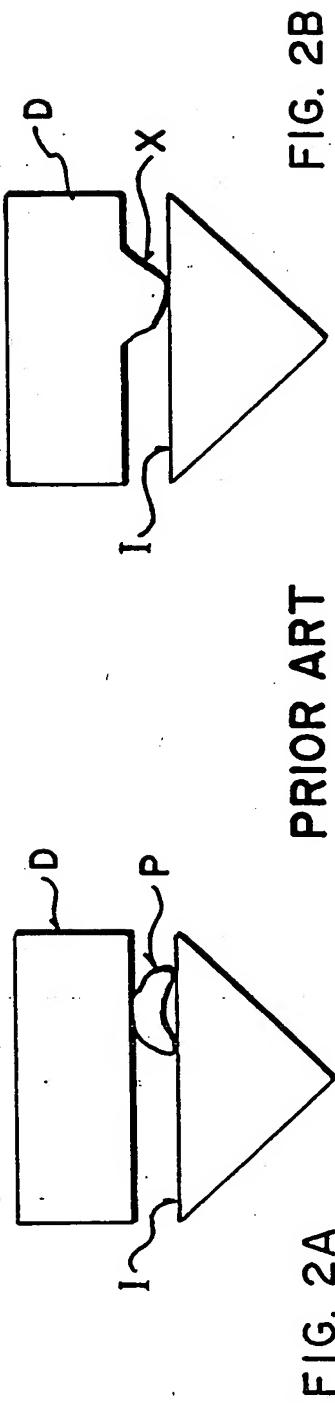
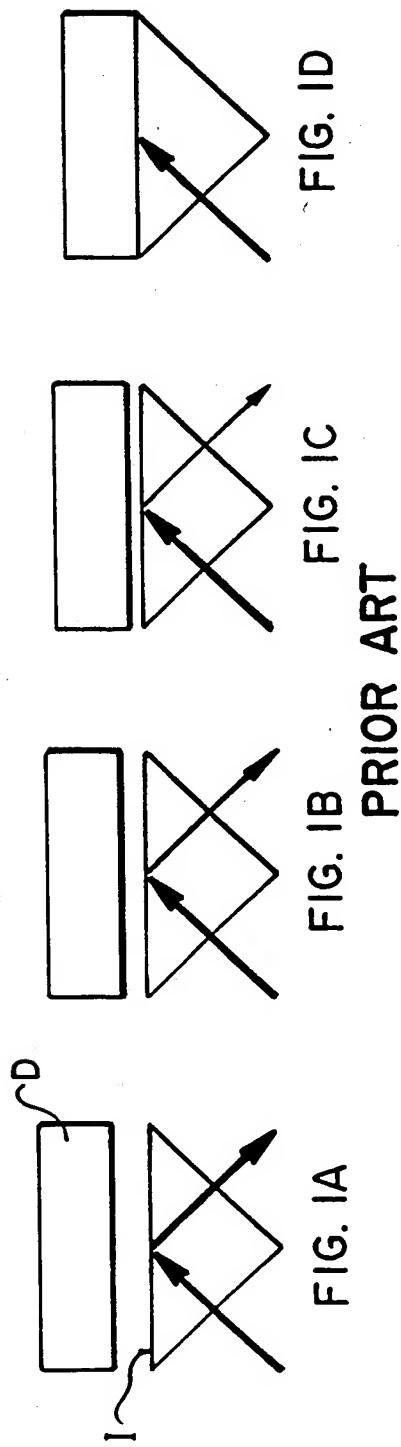
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7. A method as defined in claim 4, wherein said member is an elastomer.

8. A method as defined in claim 4, wherein said member is a silicone elastomer.

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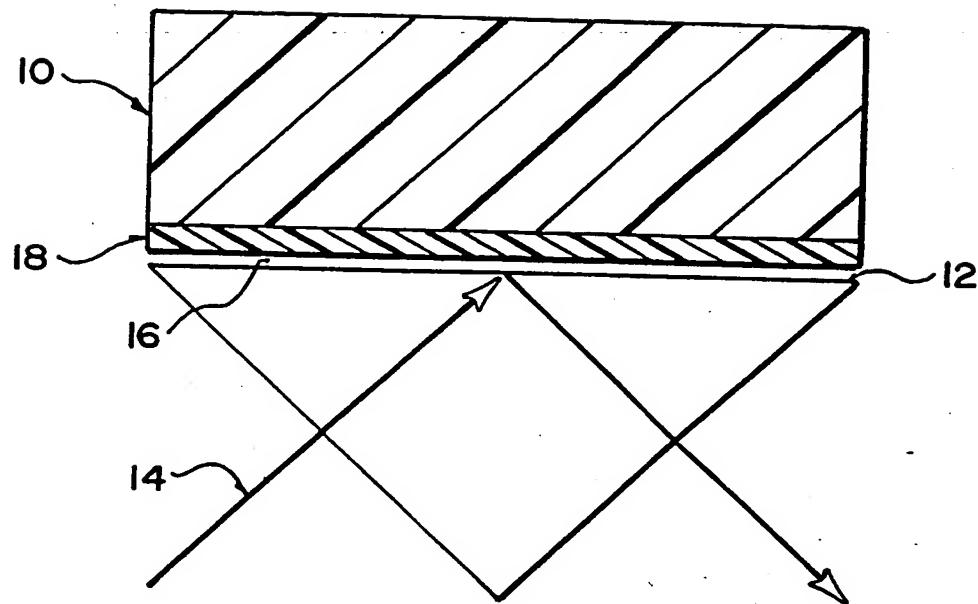


FIG. 3A

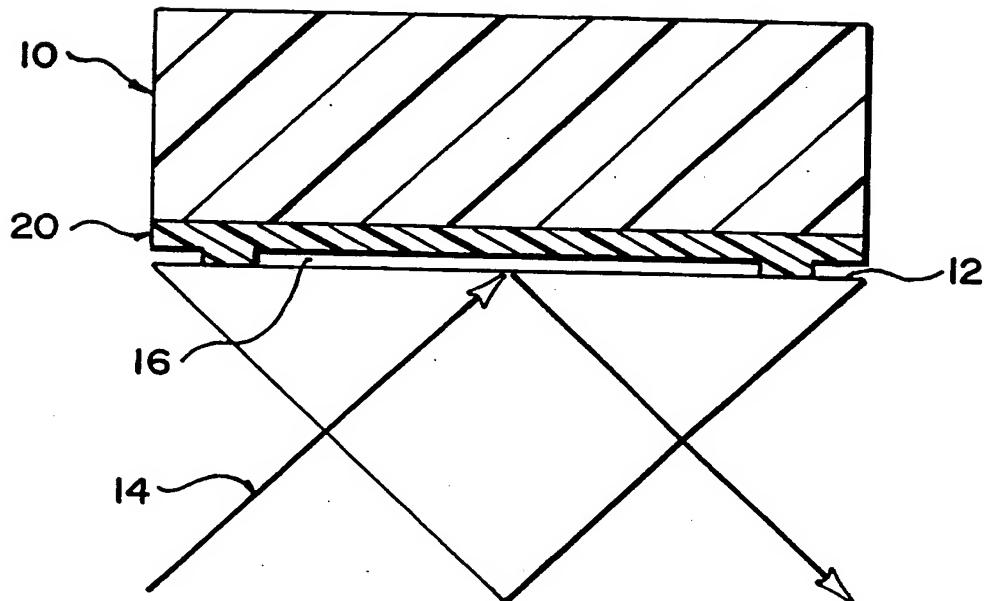


FIG. 3B

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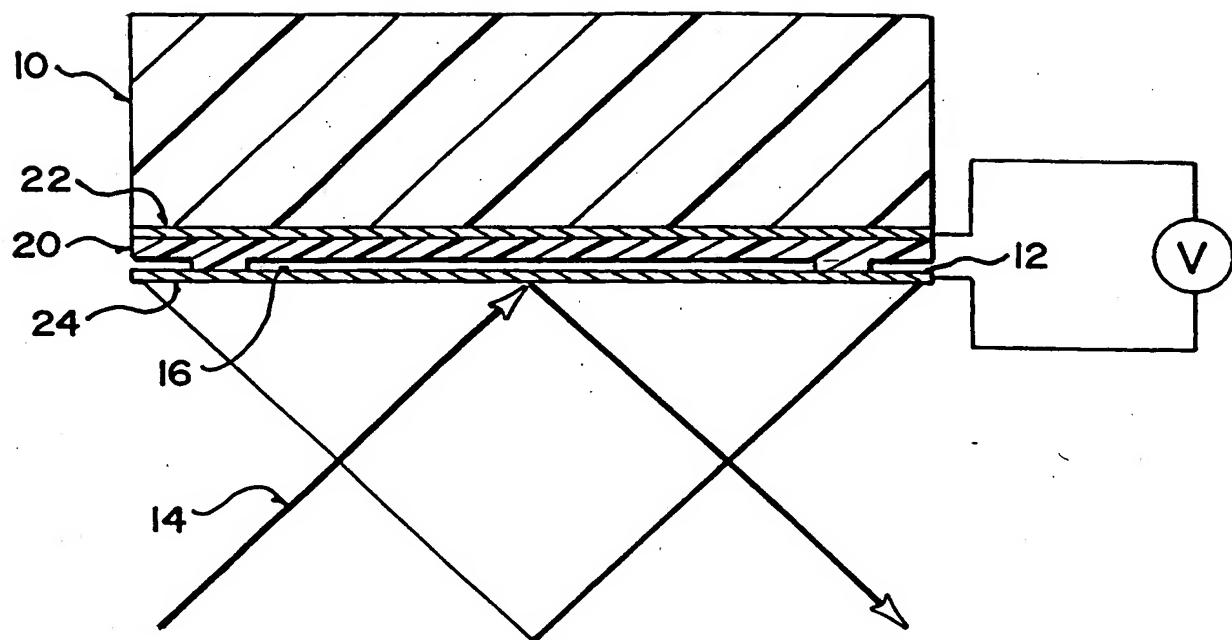


FIG. 3C

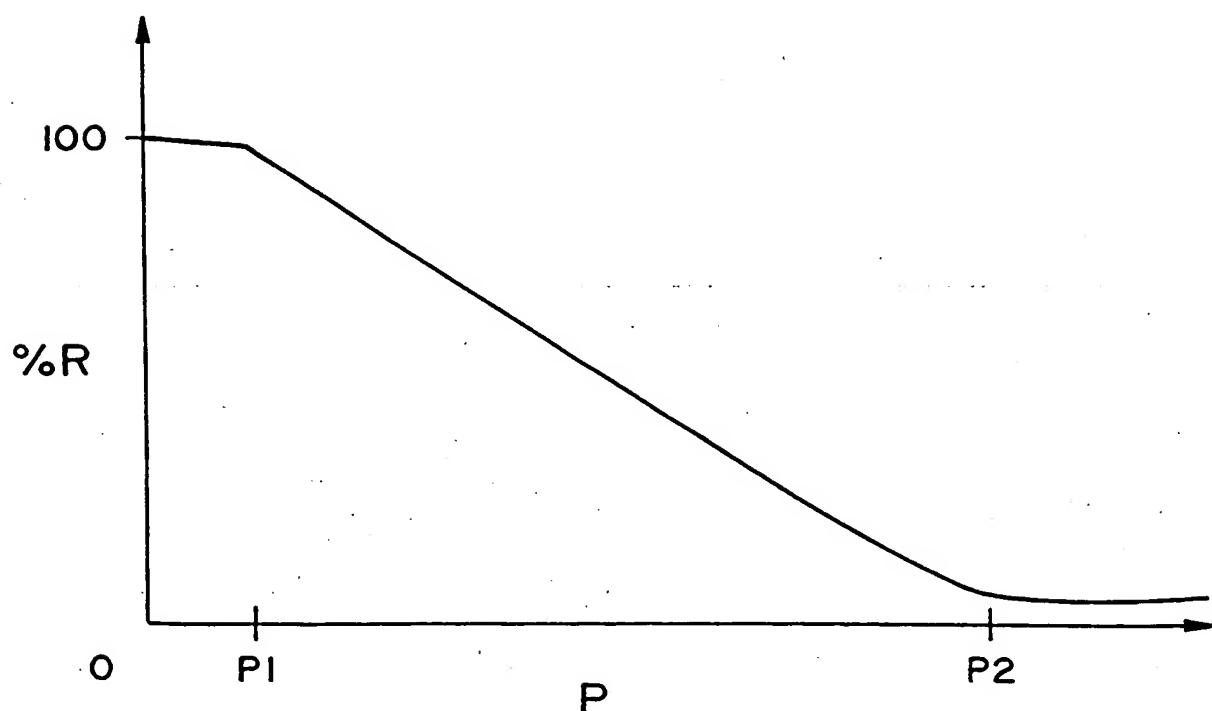


FIG. 4

# INTERNATIONAL SEARCH REPORT

Intern. 1st Application No  
PCT/CA 98/00457

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 6 G02B26/02 B29C59/16 B29D11/00 C08J5/00

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC 6 G02B G02F C08J B29C B29D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 714 326 A (CANON) 22 December 1987 see column 2, line 33 - line 43 see column 4, line 61 - column 5, line 45 ---	1-9
X	GB 2 265 024 A (BRITISH AEROSPACE) 15 September 1993 see page 6, line 03 - page 9, line 05 ---	1-9
A	US 3 291 554 A (PRICE) 13 December 1966 see column 3, line 67 - column 4, line 10; figure 8 ---	1
A	US 3 556 638 A (BANKS) 19 January 1971 see column 4, line 67 - column 5, line 75 ---	1
	-/-	

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

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Date of the actual completion of the international search

22 December 1998

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# INTERNATIONAL SEARCH REPORT

Intern:        Application No:  
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**C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT**

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	CARLSON J D ET AL: "Surface property changes induced in poly(1-hexene) elastomer by high energy ion irradiation" PROCEEDINGS OF THE FOURTH INTERNATIONAL CONFERENCE ON ION BEAM MODIFICATION OF MATERIALS, ITHACA, NY, USA, 16-20 JULY 1984, vol. B7-8, pt.2, pages 507-512, XP002072103 ISSN 0168-583X, NUCLEAR INSTRUMENTS & METHODS IN PHYSICS RESEARCH, SECTION B (BEAM INTERACTIONS WITH MATERIALS AND ATOMS), MARCH 1985, NETHERLANDS Chapter: 5. Conclusion ---	1
X	US 5 221 987 A (LAUGHLIN) 22 June 1993 see column 1, line 53 - column 2, line 09 see column 4, line 42 - line 47; figure 8 ---	1
P,X	EP 0 797 127 A (SHINETSU POLYMER CO) 24 September 1997 see claims 1-3 ---	10-13
A	EP 0 204 427 A (RAYCHEM CORP) 10 December 1986 see claim 1 ---	10
A	DATABASE WPI Section Ch, Week 7925 Derwent Publications Ltd., London, GB; Class A11, AN 79-46256B XP002088627 & JP 54 057576 A (HAYAKAWA GOMU KK) , 9 May 1979 see abstract ---	10
A	US 5 235 463 A (BROUSSOUX DOMINIQUE ET AL) 10 August 1993 see claims 1,3,6,7,12,13 ---	10
A	DE 37 20 861 A (CONTINENTAL AG) 16 March 1989 see claim 1 ---	10
A	US 5 147 519 A (LEGGE RONALD) 15 September 1992 see claims 1,4,11 ---	14
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## INTERNATIONAL SEARCH REPORT

International Application No  
PCT/CA 98/00457

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p><b>DATABASE WPI</b>  Section Ch, Week 8515  Derwent Publications Ltd., London, GB;  Class A35, AN 85-089577  XP002088740  &amp; JP 60 038130 A (ASAHI CHEM IND CO LTD)  , 27 February 1985  see abstract</p> <p>---</p>	14
A	<p><b>DATABASE WPI</b>  Section Ch, Week 8424  Derwent Publications Ltd., London, GB;  Class A32, AN 84-149562  XP002088741  &amp; JP 59 078816 A (SHOWA ELECTRIC WIRE CO LTD), 7 May 1984  see abstract</p> <p>-----</p>	14

## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/CA 98/00457

### Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1.  Claims Nos.: because they relate to subject matter not required to be searched by this Authority, namely:
  
2.  Claims Nos.: because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:
  
3.  Claims Nos.: because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

### Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

see additional sheet

1.  As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
  
2.  As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
  
3.  As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:
  
4.  No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

#### Remark on Protest

The additional search fees were accompanied by the applicant's protest.

No protest accompanied the payment of additional search fees.

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

This International Searching Authority found multiple (groups of) inventions in this international application, as follows:

1. Claims: 1-9

Apparatus for switching an interface between a total internal reflection state and a frustrated reflection state

2. Claims: 10-13

A method of stiffening portion of a member (an elastomer) by irradiating said selected portion with ultraviolet light (in the presence of oxygen).

3. Claims: 14-19

a method of stiffening selected portion of a member by applying a non-adhesive (stiff) polymer coating to a sacrificial film; applying said member to said polymer-coated film and dissolving said film.

**INTERNATIONAL SEARCH REPORT**

Information on patent family members

Internatinal Application No

PCT/CA 98/00457

Patent document cited in search report		Publication date		Patent family member(s)		Publication date
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GB 2265024	A	15-09-1993		NONE		
US 3291554	A	13-12-1966		NONE		
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			FR	2010148 A	13-02-1970	
			GB	1237655 A	30-06-1971	
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			JP	4301801 A	26-10-1992	
DE 3720861	A	16-03-1989		NONE		
US 5147519	A	15-09-1992		NONE		



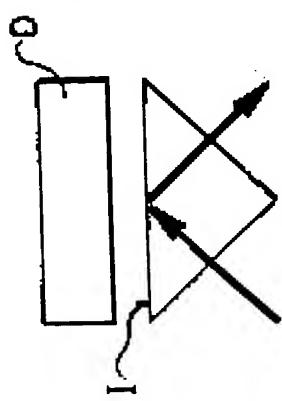


FIG. 1A  
PRIOR ART

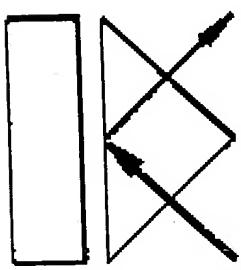


FIG. 1B  
PRIOR ART

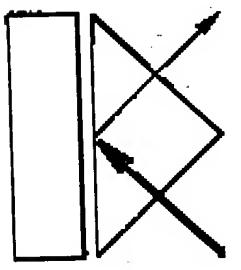


FIG. 1C  
PRIOR ART

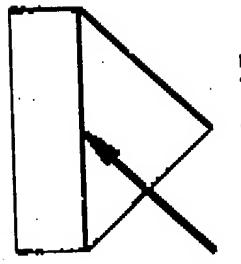


FIG. 1D  
PRIOR ART

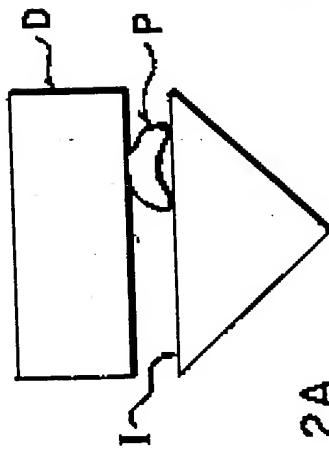


FIG. 2A

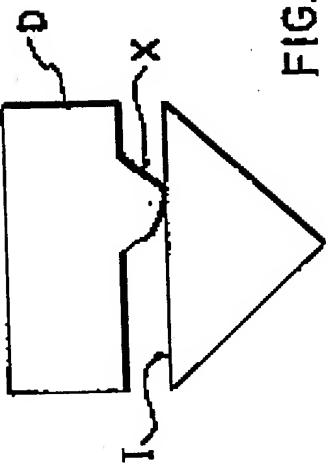


FIG. 2B

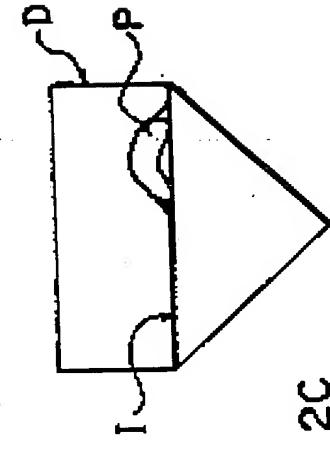


FIG. 2C

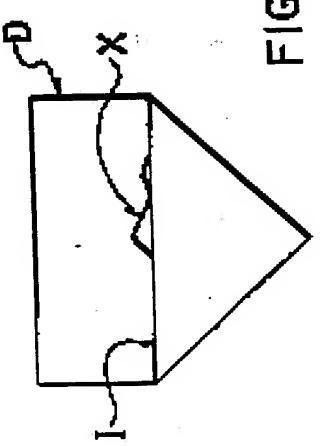


FIG. 2D

PRIOR ART

PRIOR ART

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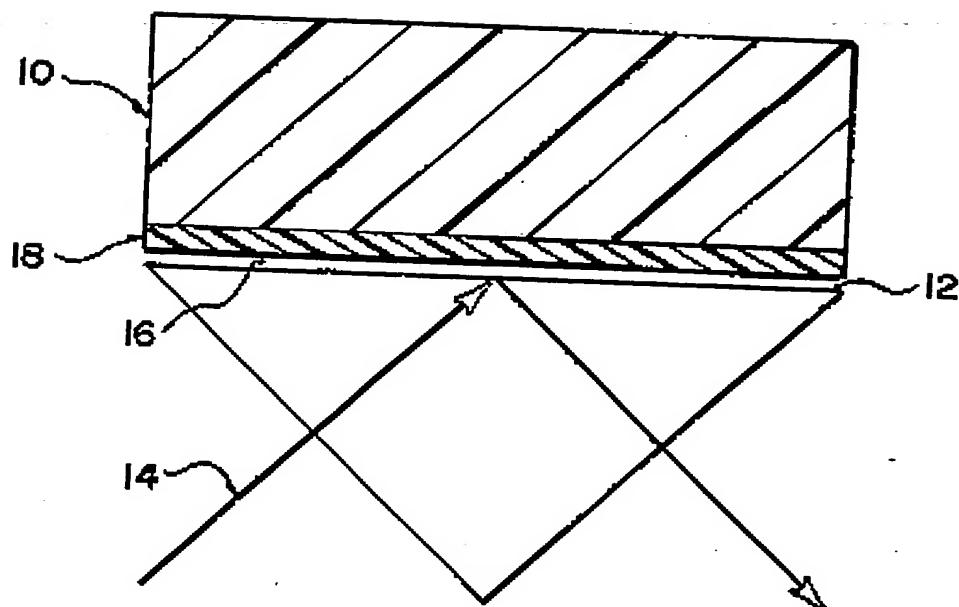


FIG. 3A

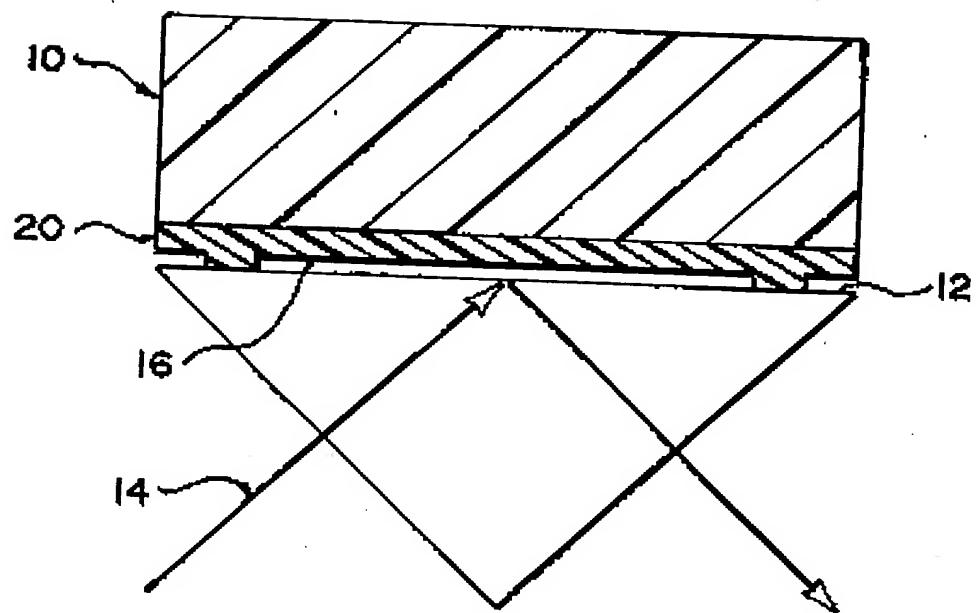


FIG. 3B

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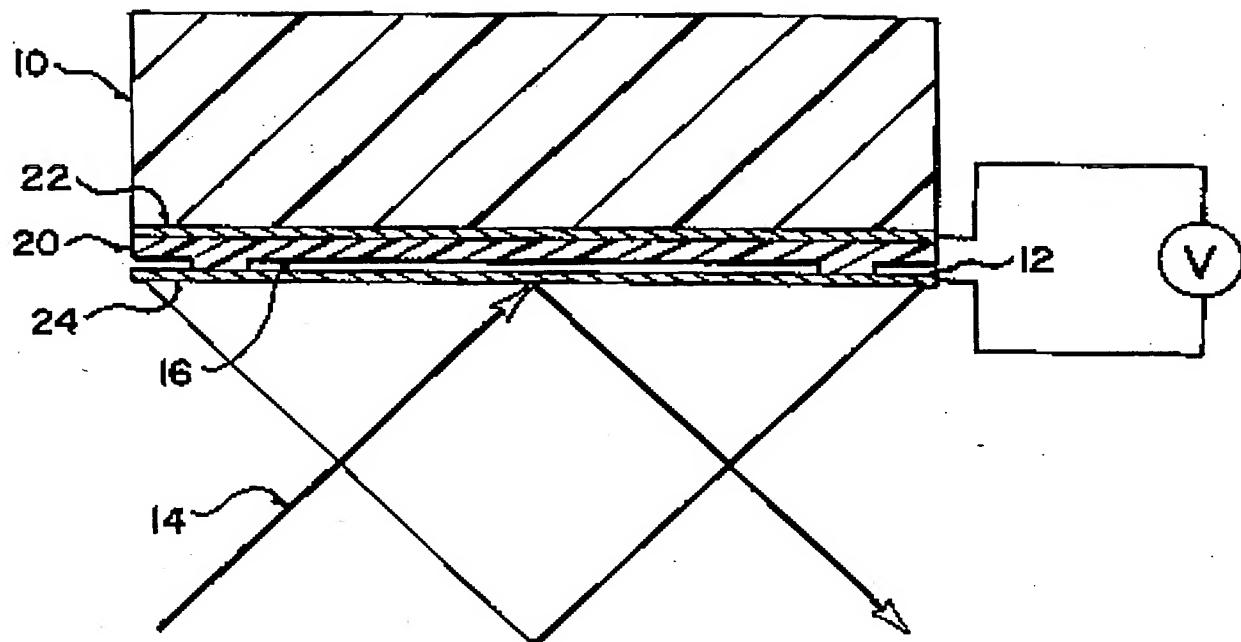


FIG. 3C

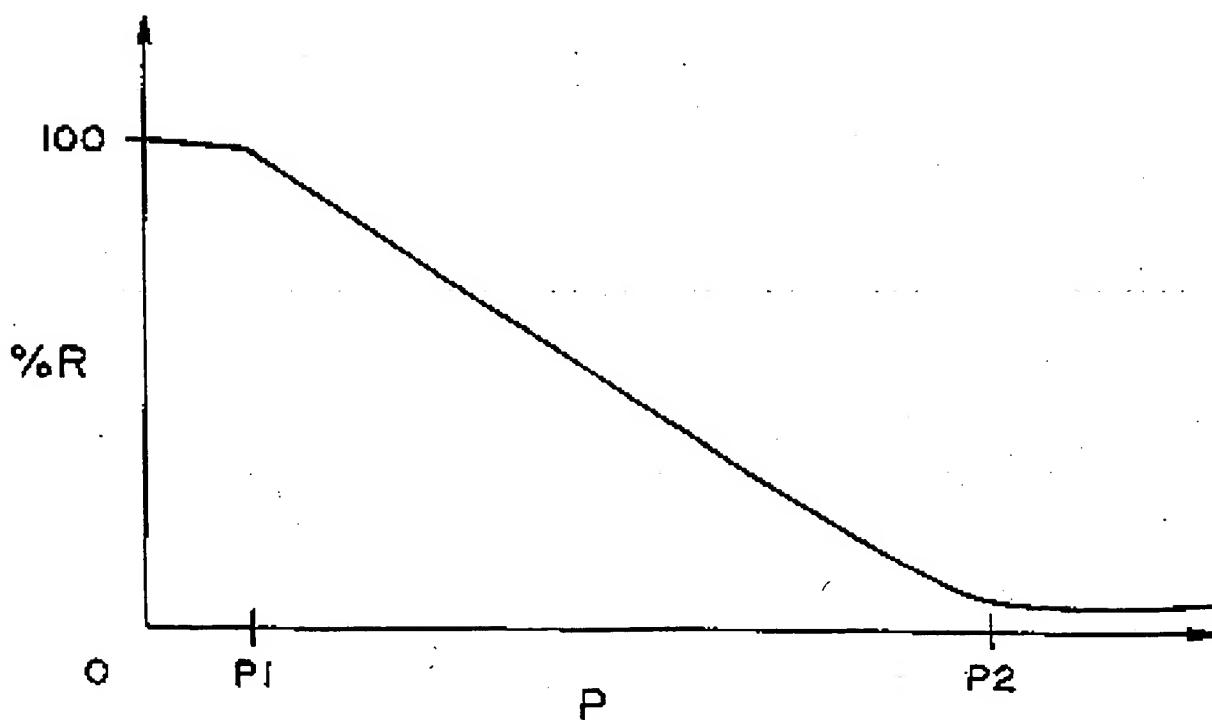


FIG. 4

